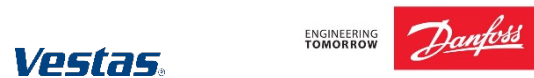


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CHARACTERIZING THE REACTIVE POWER CAPABILITY OF WIND FARM COLLECTOR NETWORKS

Nawaf Nazir, Ian Hiskens, and Mads Rønne Almassalkhi*



malmassa@uvm.edu
mads.almassalkhi@pnnl.gov



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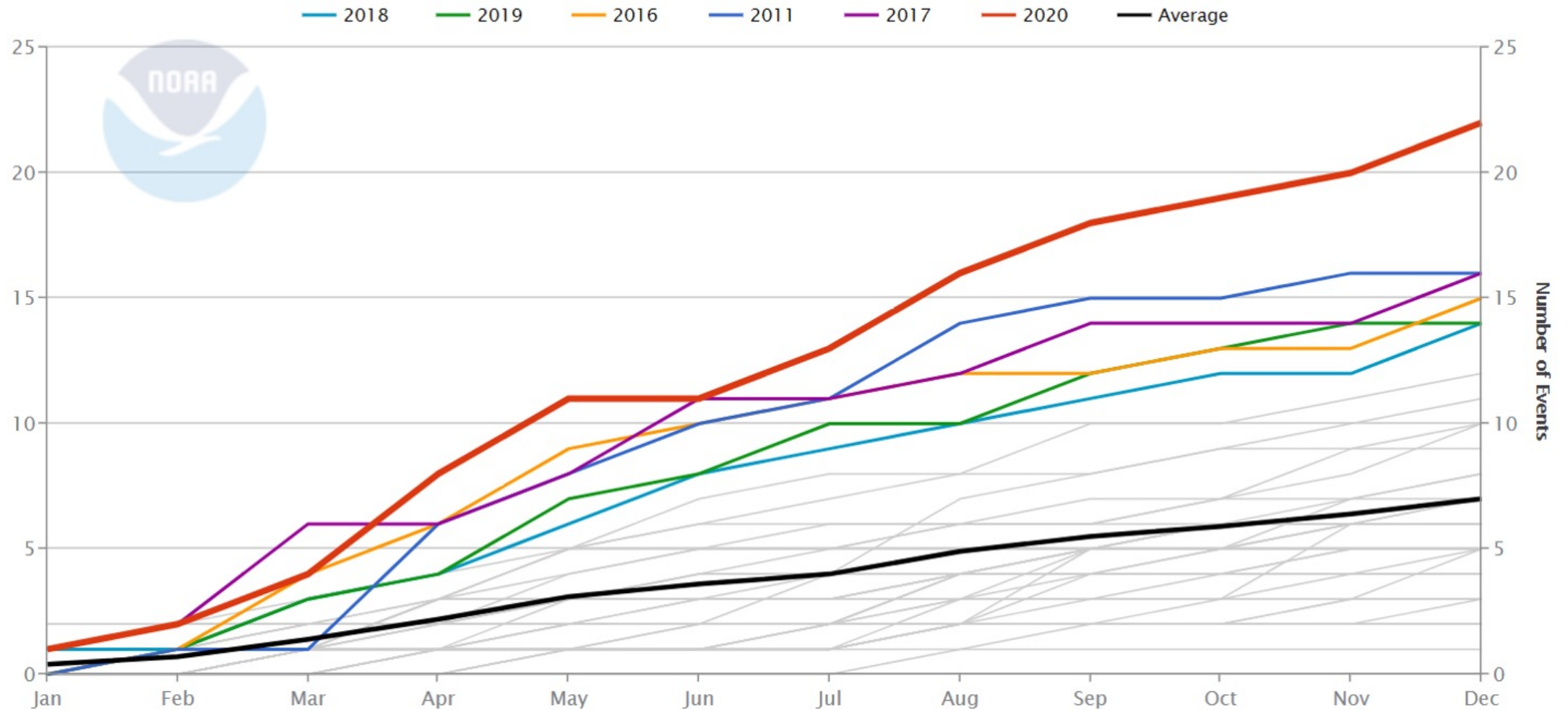
[@theEnergyMads](https://twitter.com/theEnergyMads)



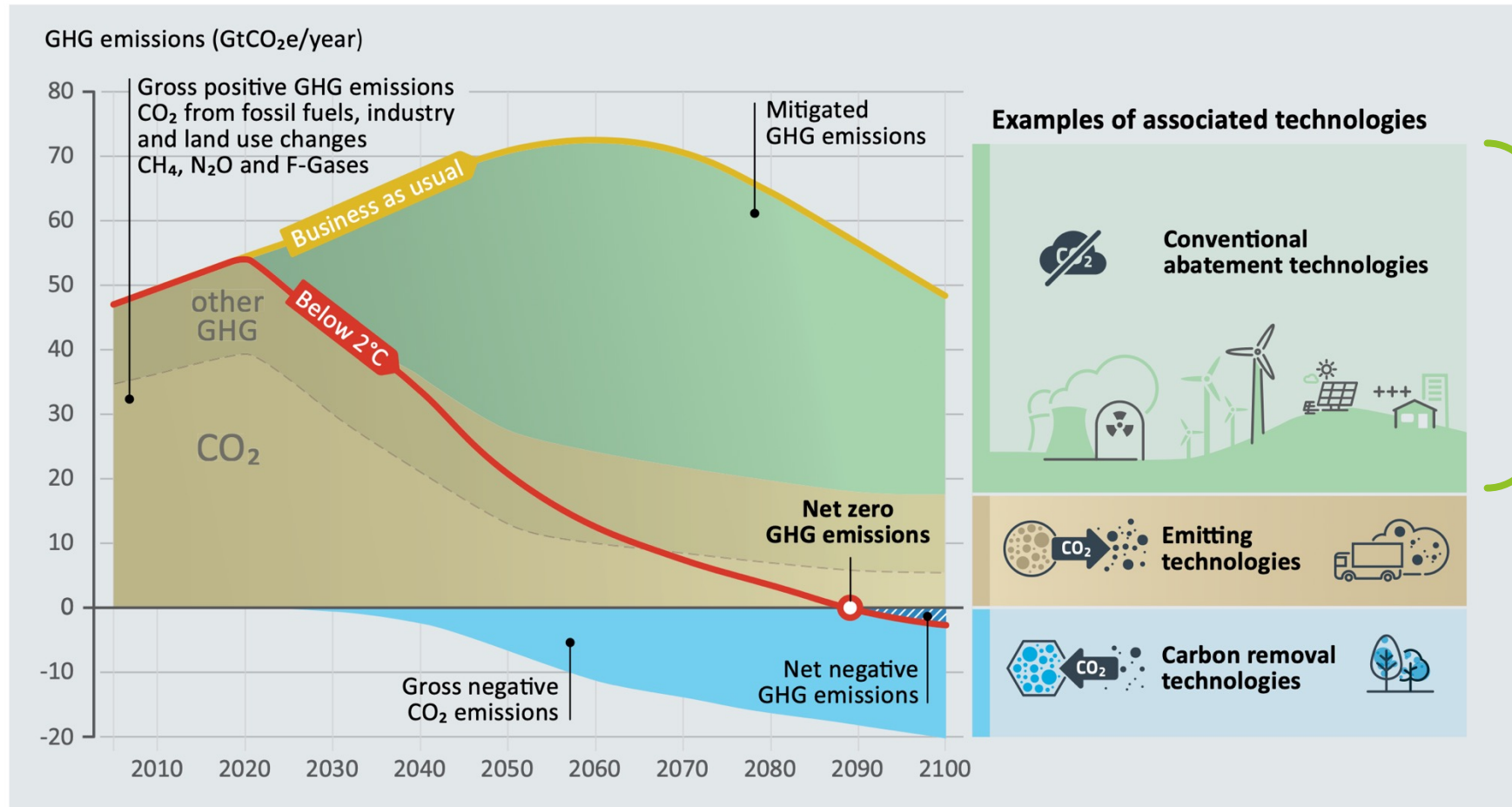
<https://madsalma.github.io>

Climate challenges are real

1980–2020 Year-to-Date United States Billion-Dollar Disaster Event Count (CPI-Adjusted)



Solutions? If they work, they will matter!



Requires massive
TW-scale
renewable
integration

A massive
power systems
problem!

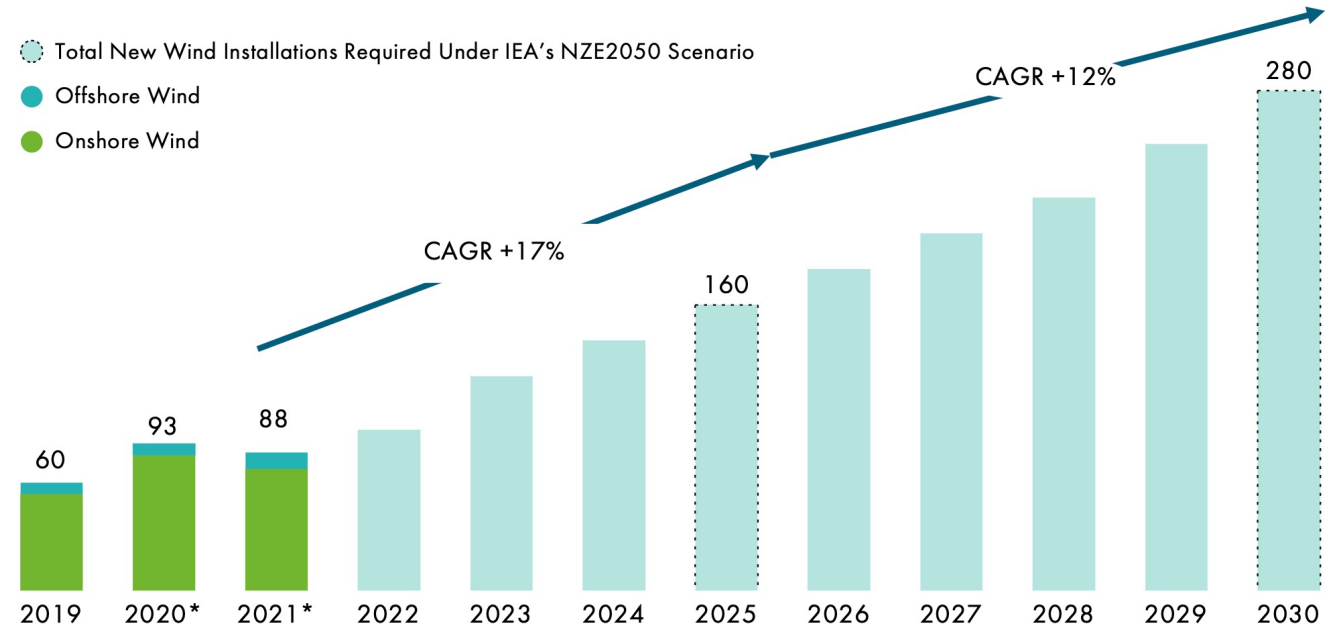


The answer is blowing in the wind...



Source: wikipedia

Annual wind installations must increase dramatically to reach net zero by 2050
New global wind installations (GW)

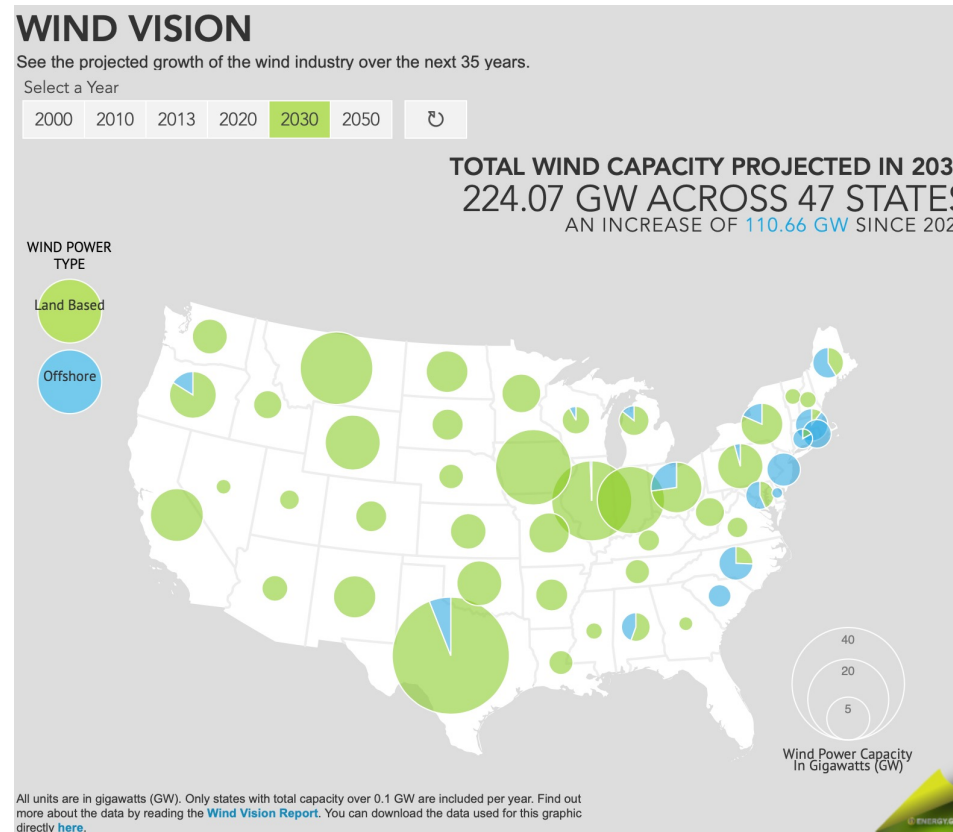


Source: GWEC Market Intelligence; IEA World Energy Outlook (2020), volume in 2022-2024 and 2026-2029 are estimates

The answer is blowing in the wind...



Source: wikipedia



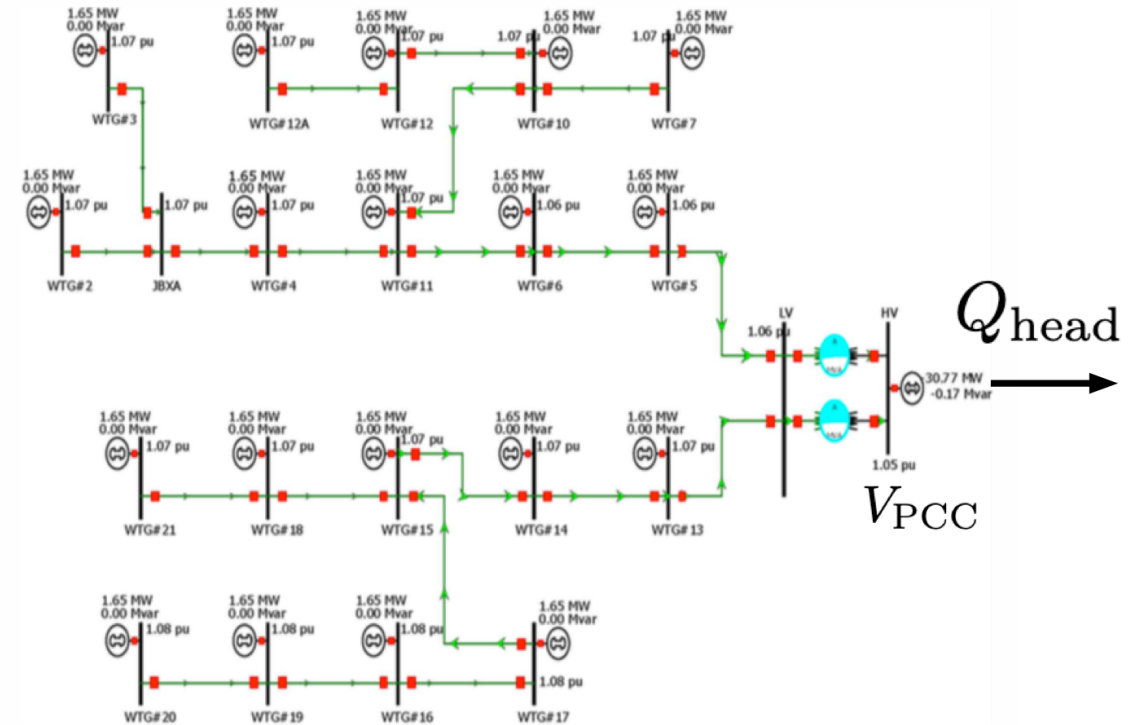
Source: <https://www.energy.gov/eere/wind/wind-vision>

US will double
its wind capacity
between 2020
and 2030



More wind generation, more reliability issues

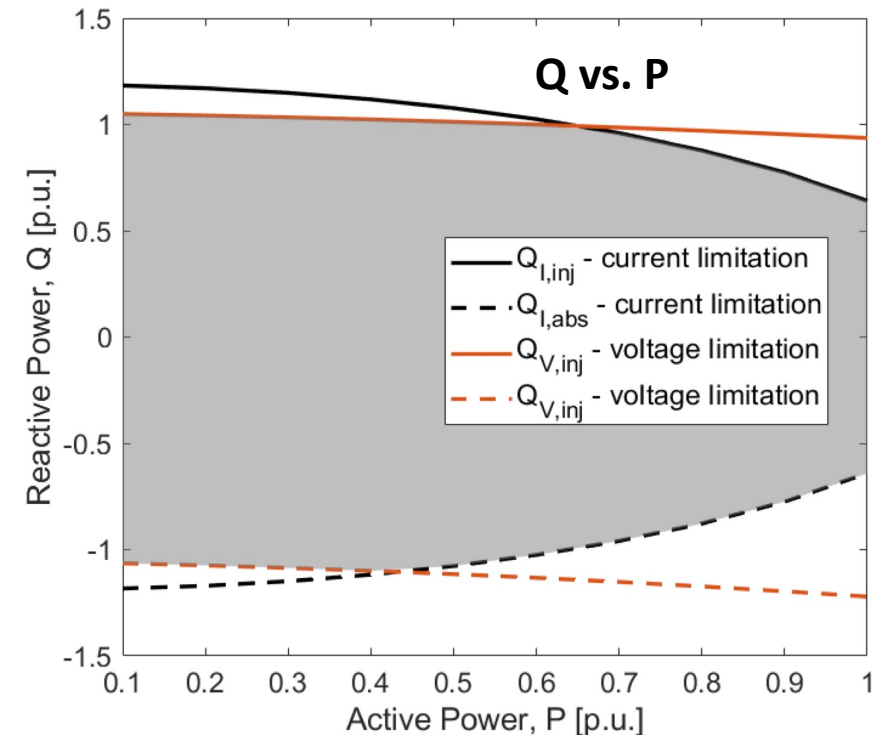
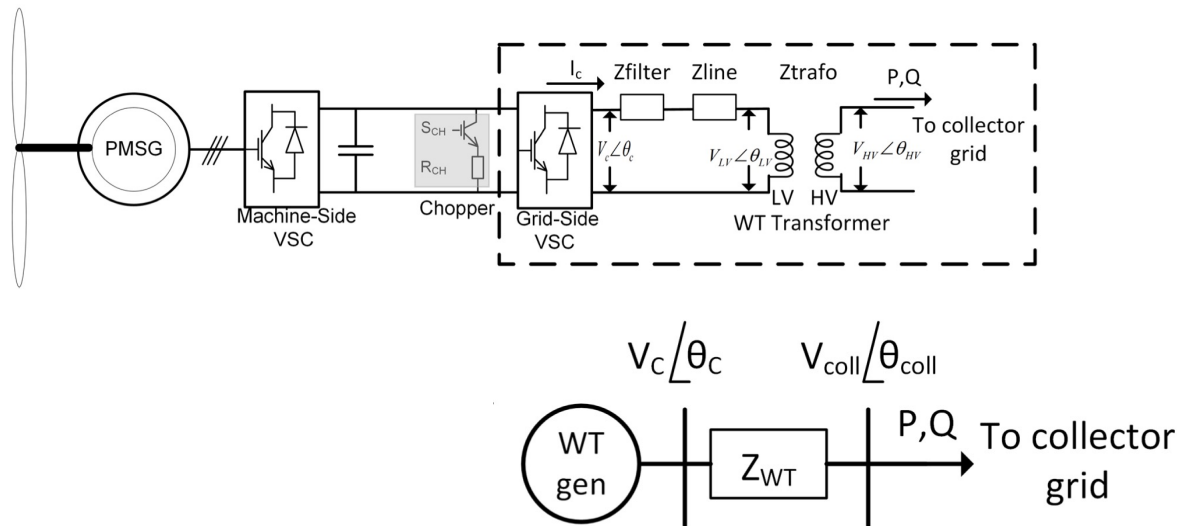
- Wind farms must take an active role in regulate voltage at interconnection points with transmission systems
- Reactive power support from wind farm networks is important for reliability.
- **Question:** How much reactive power support can a wind farm offer?



Reactive power capability of a single WT

- We understand reactive power support from a single WT well

Type 4 WT with its single-line diagram & reactive power capability:

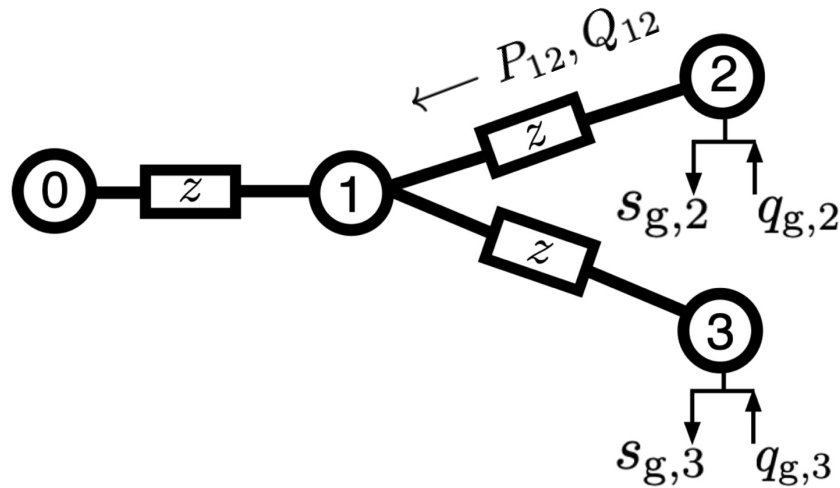


Reactive power capability of a wind farm

- Simple idea: just aggregate reactive power capability curves from N WTs
 - Overestimates reactive power support from wind farm due to network constraints
 - Protection systems will automatically limit reactive power when network limits are reached
- A better idea
 - Explicitly consider the wind farm collector network and AC physics and find *maximum reactive power injection limits* for given active power generation
 - **Technical challenge:** this is a nonconvex optimization problem (NP-hard)

Reactive power capability of a wind farm

- Simple 3-node, 2-WT collector network represented by *DistFlow* model:



$$v_i := |V_i|^2 \text{ and } l_{ij} := |I_{ij}|^2$$

$$v_j = v_i + 2r_{ij}P_{ij} + 2x_{ij}Q_{ij} - |z_{ij}|^2 l_{ij}$$

$$P_{ij} = p_j + \sum_{h:h \rightarrow j} (P_{jh} - r_{jh}l_{jh})$$

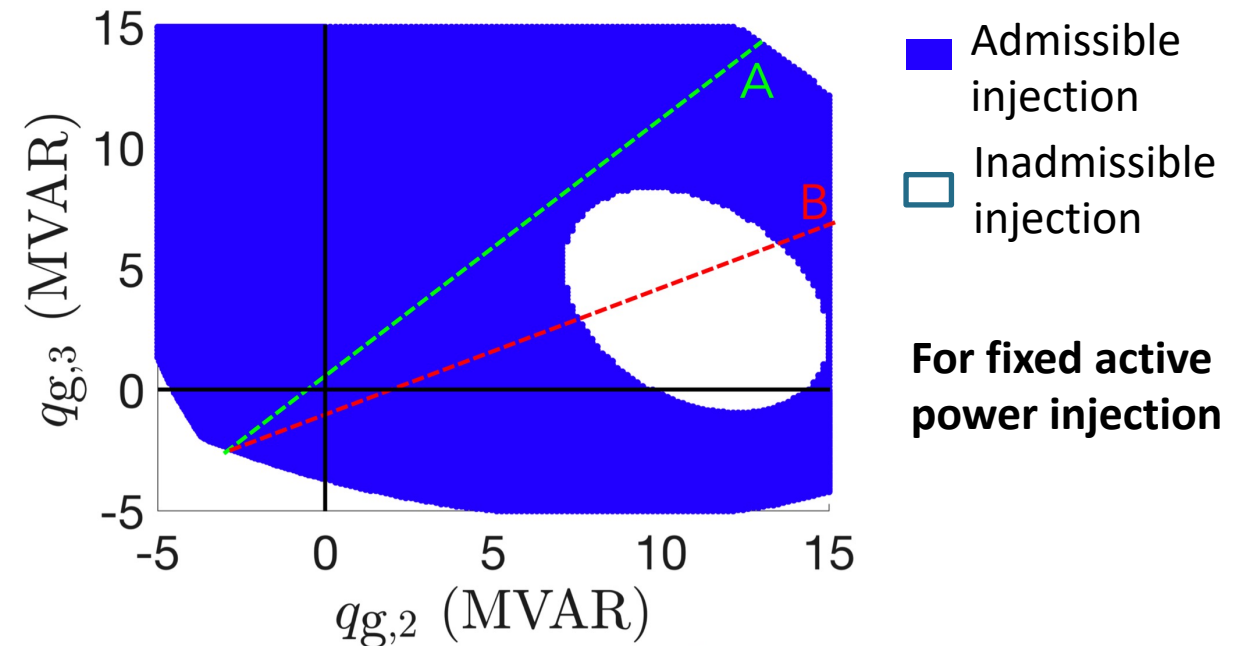
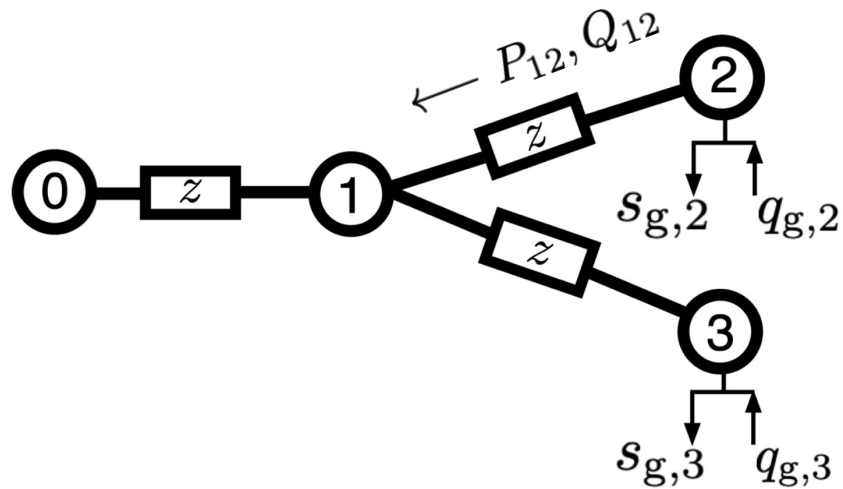
$$Q_{ij} = q_j + \sum_{h:h \rightarrow j} (Q_{jh} - x_{jh}l_{jh})$$

$$l_{ij}(P_{ij}, Q_{ij}, v_j) = \frac{P_{ij}^2 + Q_{ij}^2}{v_j}, \text{ The only non-convex constraint}$$

$$\text{Network limits: } v_i \in [\underline{v}_i, \bar{v}_i], l_{ij} \in [\underline{l}_{ij}, \bar{l}_{ij}]$$

Reactive power capability of a wind farm

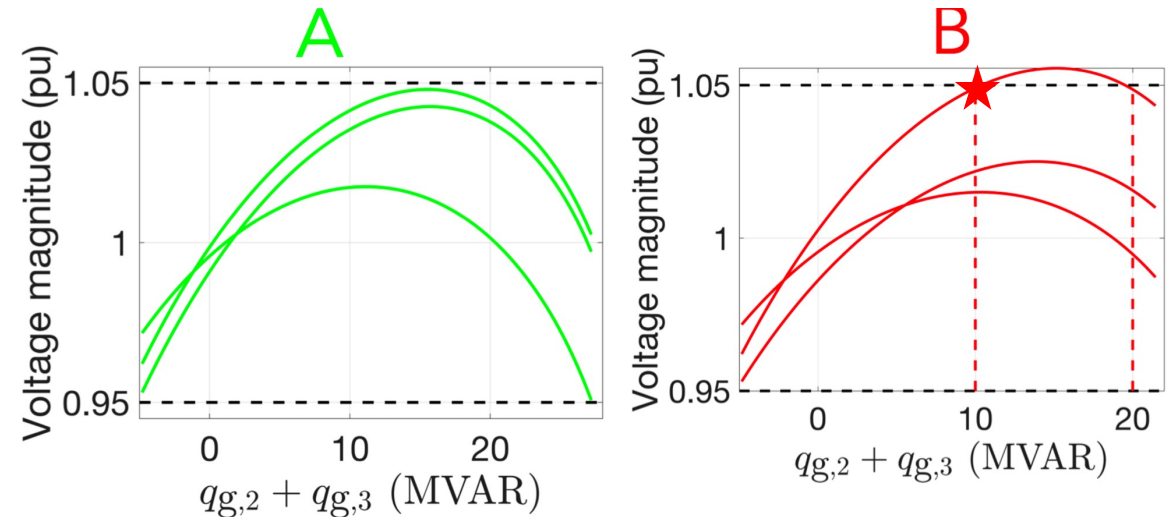
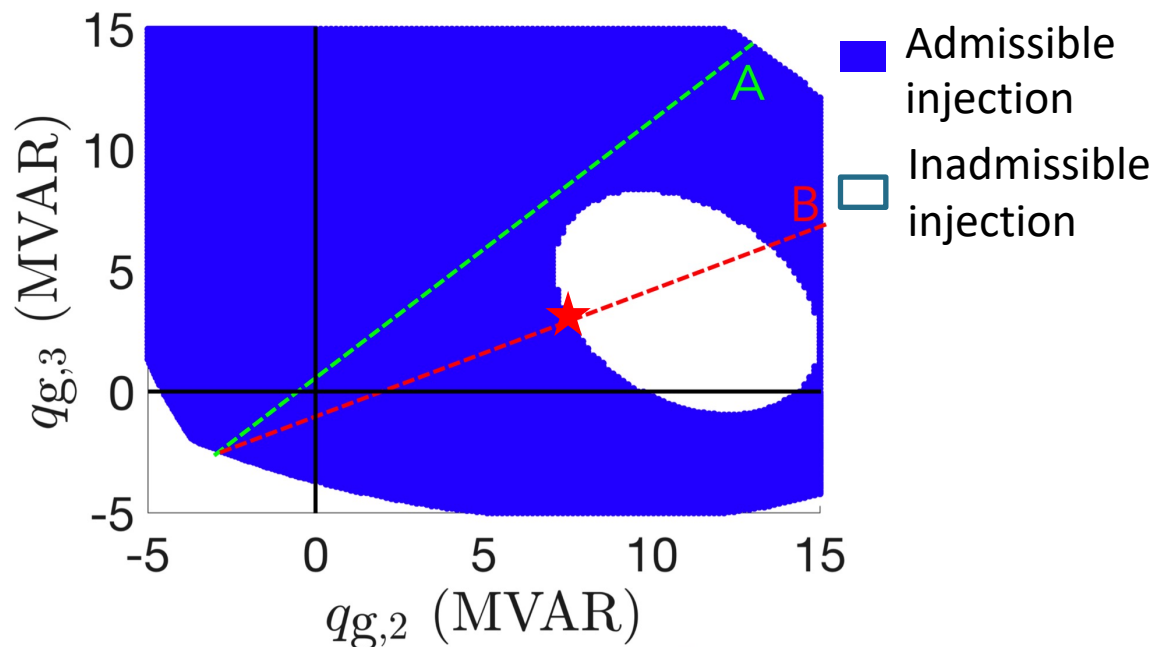
- Simple 3-node, 2-WT collector network represented by *DistFlow* model:



Network limits: $v_i \in [\underline{v}_i, \bar{v}_i], l_{ij} \in [\underline{l}_{ij}, \bar{l}_{ij}]$

Reactive power capability of a wind farm

- Simple 3-node, 2-WT collector network represented by *DistFlow* model:

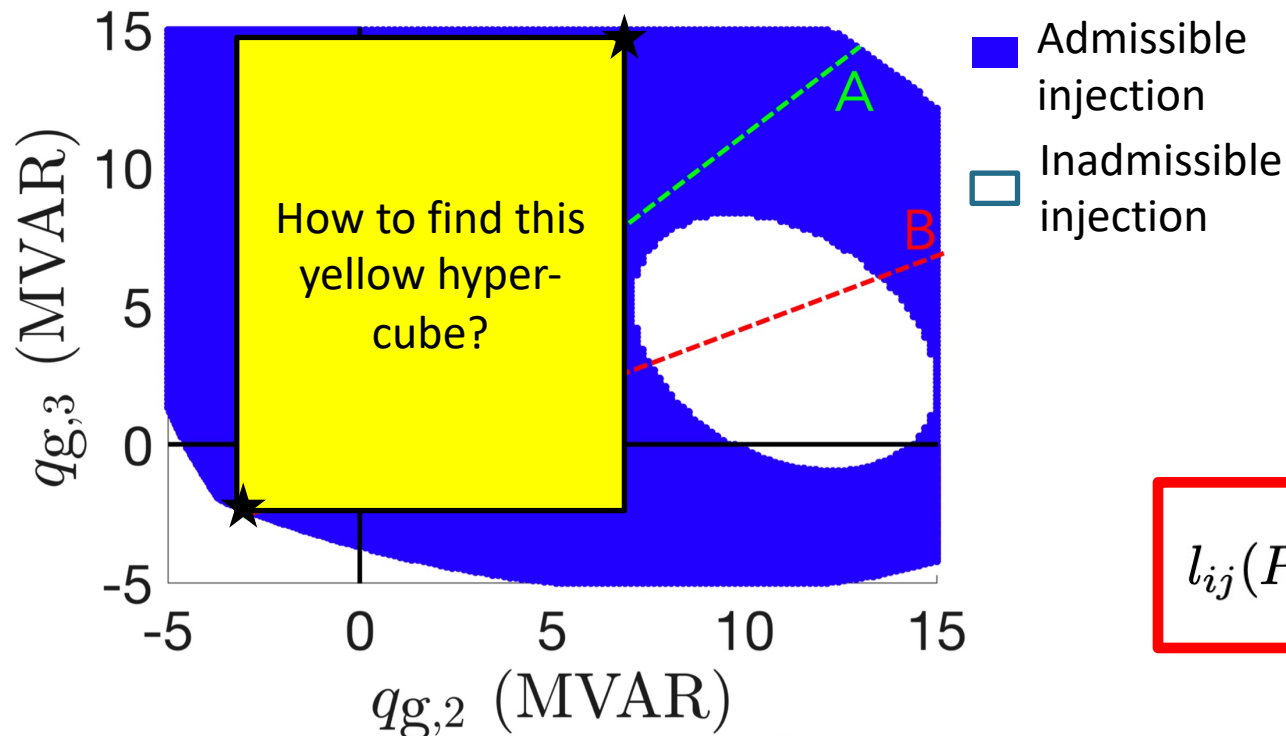


The two WTs reactive power outputs are limited in aggregate by the network – i.e., their individual limits are coupled

Network limits: $v_i \in [\underline{v}_i, \bar{v}_i], l_{ij} \in [\underline{l}_{ij}, \bar{l}_{ij}]$

Reactive power capability of a wind farm

- **Goal:** find largest rectangle to get Q-limits for each WT (decouple)



$$v_j = v_i + 2r_{ij}P_{ij} + 2x_{ij}Q_{ij} - |z_{ij}|^2 l_{ij}$$

$$P_{ij} = p_j + \sum_{h:h \rightarrow j} (P_{jh} - r_{jh}l_{jh})$$

$$Q_{ij} = q_j + \sum_{h:h \rightarrow j} (Q_{jh} - x_{jh}l_{jh})$$

$$l_{ij}(P_{ij}, Q_{ij}, v_j) = \frac{P_{ij}^2 + Q_{ij}^2}{v_j}$$

Idea: replace non-convex constraint with a convex envelope

Convex inner approximation via proxy variables

If we can find bounds $l_{lb,ij} \leq l_{ij}(P_{ij}, Q_{ij}, v_j) = \frac{P_{ij}^2 + Q_{ij}^2}{v_j} \leq l_{ub,ij}$

Then, we can create proxy variables that upper (+) and lower (-) bound the actual (P, Q, V)

$$P^+ := Cp - D_R l_{lb}$$

$$P^- := Cp - D_R l_{ub}$$

$$Q^+ := Cq - D_{X_+} l_{lb} - D_{X_-} l_{ub}$$

$$Q^- := Cq - D_{X_+} l_{ub} - D_{X_-} l_{lb}$$

$$V^+ := v_0 \mathbf{1}_n + M_p p + M_q q - H_+ l_{lb} - H_- l_{ub}$$

$$V^- := v_0 \mathbf{1}_n + M_p p + M_q q - H_+ l_{ub} - H_- l_{lb}$$

Given any nominal operating point, $x_{ij}^0 := (P_{ij}^0, Q_{ij}^0, v_j^0)$

we can construct a 2nd order Taylor-series expansion:

$$l_{ij} \approx l_{ij}^0 + \mathbf{J}_{ij}^\top \delta_{ij} + \frac{1}{2} \delta_{ij}^\top \mathbf{H}_{e,ij} \delta_{ij}$$

and from this model, we can use proxy vars to **explicitly** define upper and lower bounds

Convex inner approximation via proxy variables

If we can find bounds $l_{lb,ij} \leq \boxed{l_{ij}(P_{ij}, Q_{ij}, v_j) = \frac{P_{ij}^2 + Q_{ij}^2}{v_j}} \leq l_{ub,ij}$

Then, we can create proxy variables that upper (+) and lower (-) bound the actual (P, Q, V)

$$l_{lb,ij} := f_{lb,ij}(P_{ij}^-, Q_{ij}^-, v_j^-, P_{ij}^+, Q_{ij}^+, v_j^+, x_{ij}^0) \leq l_{ij} \leq f_{ub,ij}(P_{ij}^-, Q_{ij}^-, v_j^-, P_{ij}^+, Q_{ij}^+, v_j^+, x_{ij}^0) \leq l_{ub,ij}$$

Has been shown to be **affine**

Has been shown to be **convex** (SOC)

For mathematical details, please see:

Nawaf Nazir and Mads Almassalkhi. "Grid-aware aggregation and realtime disaggregation of distributed energy resources in radial networks." (Under review, IEEE Transactions, Rev 02).



Convex inner approximation via proxy variables

$$P^+ := Cp - D_R l_{lb}$$

$$P^- := Cp - D_R l_{ub}$$

$$Q^+ := Cq - D_{X_+} l_{lb} - D_{X_-} l_{ub}$$

$$Q^- := Cq - D_{X_+} l_{ub} - D_{X_-} l_{lb}$$

$$V^+ := v_0 \mathbf{1}_n + M_p p + M_q q - H_+ l_{lb} - H_- l_{ub}$$

$$V^- := v_0 \mathbf{1}_n + M_p p + M_q q - H_+ l_{ub} - H_- l_{lb}$$

$$0 \leq l_{lb,ij} := f_{lb,ij}(P_{ij}^-, Q_{ij}^-, v_j^-, P_{ij}^+, Q_{ij}^+, v_j^+, x_{ij}^0)$$

$$f_{ub,ij}(P_{ij}^-, Q_{ij}^-, v_j^-, P_{ij}^+, Q_{ij}^+, v_j^+, x_{ij}^0) \leq l_{ub,ij} \leq \bar{l}_{ij}$$

$$\underline{V} \leq V^-, V^+ \leq \bar{V}$$

$$\underline{q}_i \leq q_i \leq \bar{q}_i$$

Current limits

Voltage limits

WT reactive power limits

Feasible set of
convex inner
approximation

$$\mathcal{X}(x^0)$$

is
convex

Find network's reactive power capability

q_i^+ maximum reactive power limits at *each* WT, where

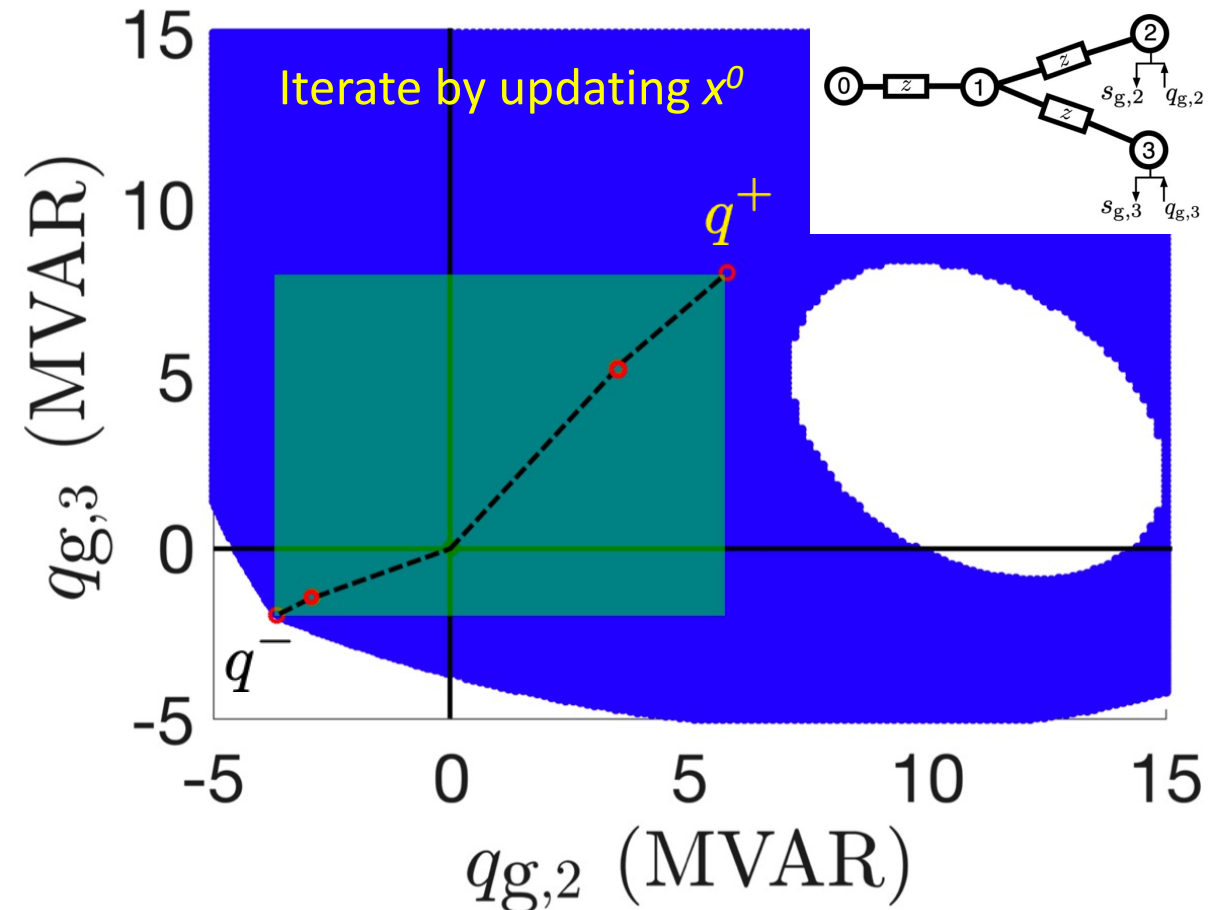
$$q^+(x^0) = \arg \max_q Q_{10}^-$$

s.t. $q \in \mathcal{X}(x^0)$

q_i^- minimum reactive power limit at *each* WT, where

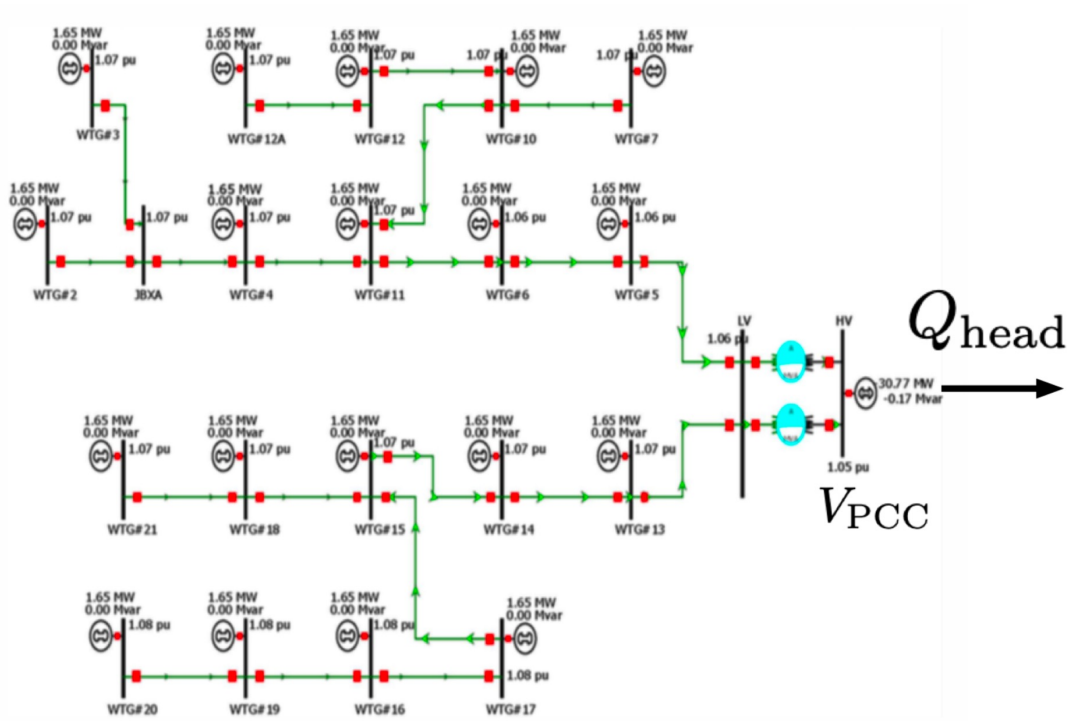
$$q^-(x^0) = \arg \min_q Q_{10}^+$$

s.t. $q \in \mathcal{X}(x^0)$

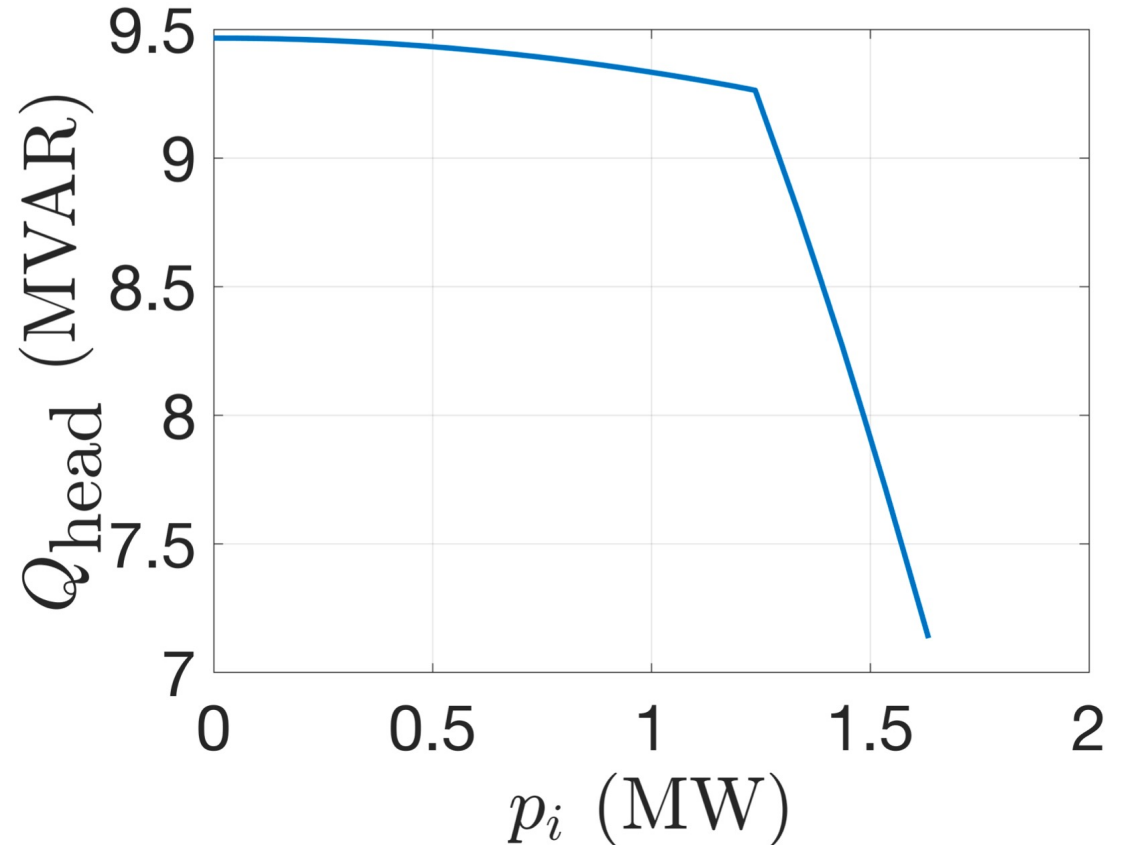




Finding network's reactive power capability

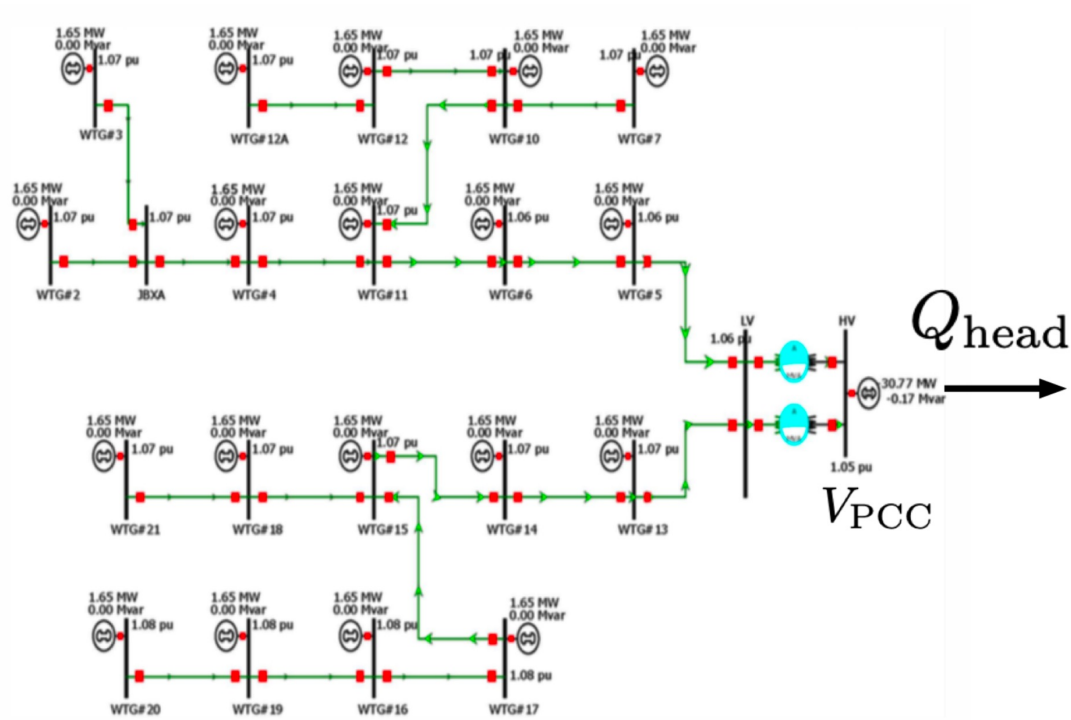


Farm has 19 WTs. Each turbine is rated at 1.65MW, [-0.5, 0.5] MVar



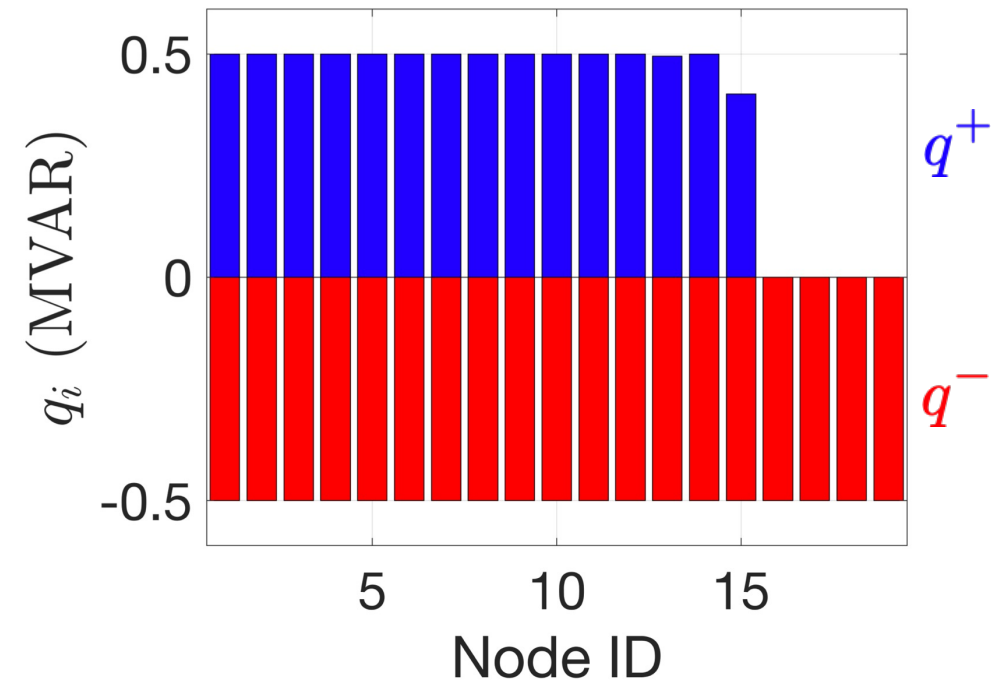


Finding network's reactive power capability



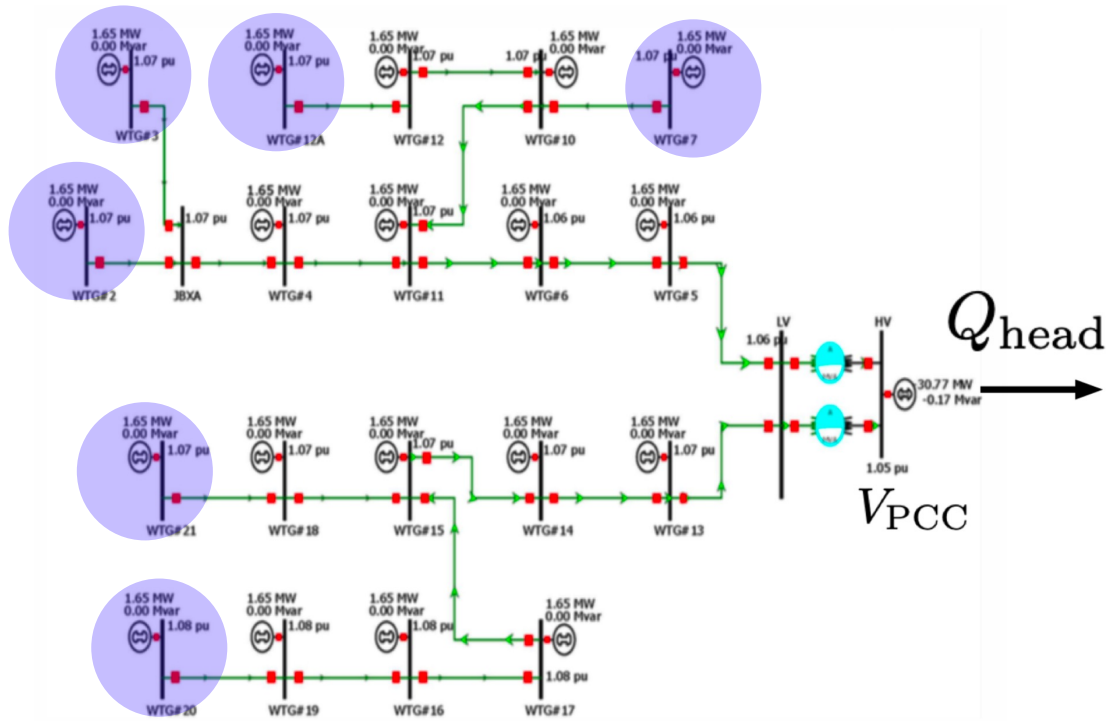
Farm has 19 WTs. Each turbine is rated at 1.65MW, [-0.5, 0.5] MVar

Scenario 1: all WTs at rated active power



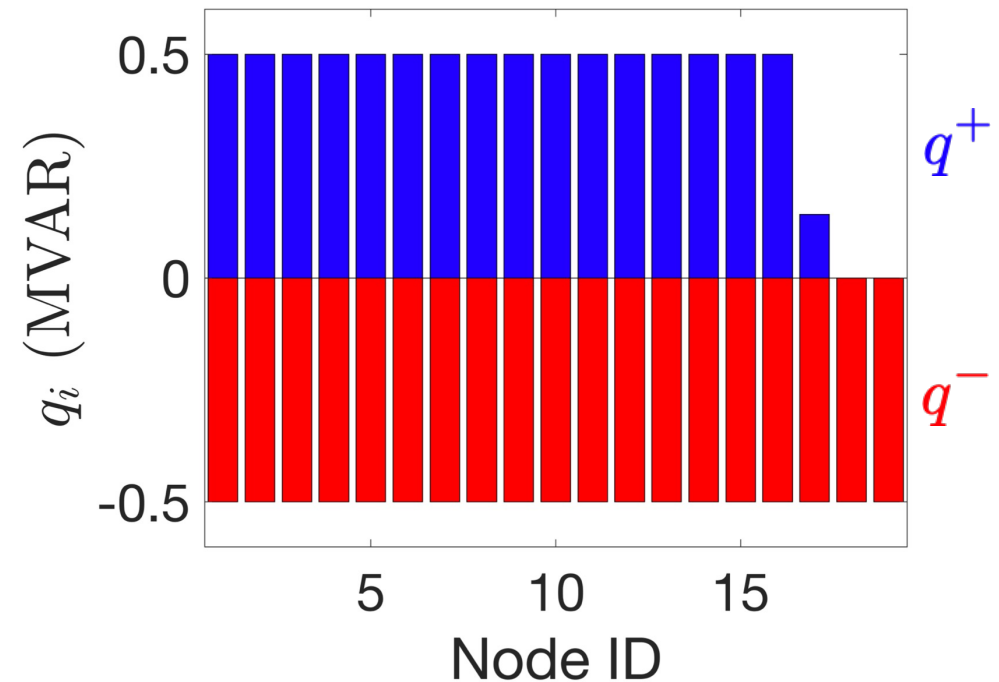


Finding network's reactive power capability

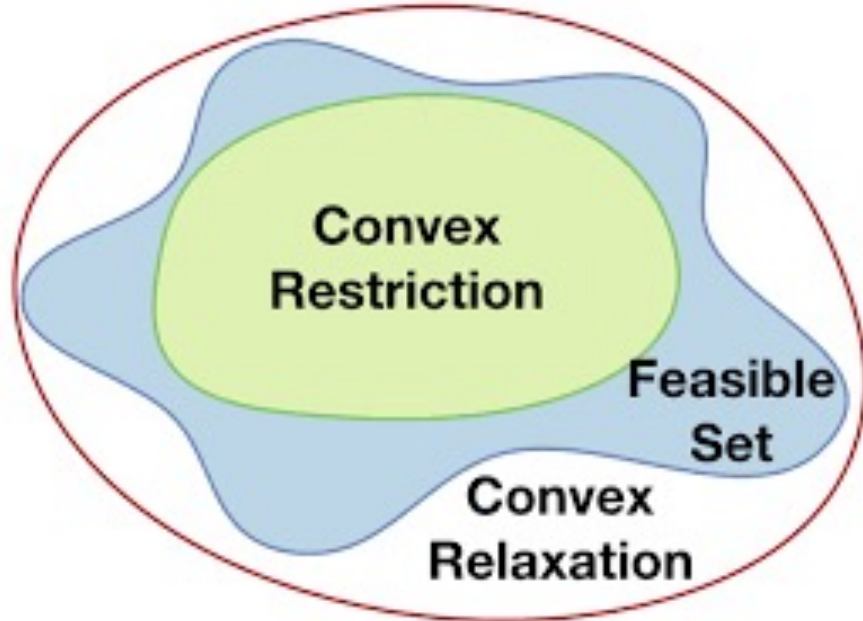


Farm has 19 WTs. Each turbine is rated at 1.65MW, [-0.5, 0.5] MVar

Scenario 2: some WTs at rated power; rest 0



Is convex restriction overly conservative?



| Scheme | Scenario 1 | Scenario 2 |
|------------|------------|------------|
| CIA-based | [-9.9,7.0] | [-9.8,7.9] |
| Nonlinear | [-9.9,7.0] | [-9.8,7.9] |
| Relaxation | [-9.9,9.1] | [-9.8,9.3] |

Relaxation over-estimates maximum reactive power capability (not surprising).

Nonlinear has no optimality guarantees AND does not guarantee that entire range is admissible (i.e., no holes)

Proposed CIA-based method is not overly conservative and formulation is convex (so range is admissible)

Next steps

- Design and test real-time network-aware WT controllers
- Study collector network topology vs. reactive power capability
- Compare methods with state-of-the-art
- Consider protection systems and real-world collector networks



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THANK YOU FOR ATTENDING! QUESTIONS? COMMENTS?

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